



CONTROL VALVES (INTRODUCTION, SELECTING & SIZING)

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AGENDA

- 1. Valve body types
- 2. Control valves
- 3. Control valve behaviors
- 4. Control valve problems
- 5. Control valve sizing
- 6. Actuators
- 7. Positioners
- 8. Valve Accessory
- 9. Valve materials
- 10. Control valve selection





1. VALVE BODY TYPES

- Sliding stem valves
 - Globe valves
 - Single seat globe valve
 - Double seat globe valve
 - 3-way globe valve
 - Needle valve
 - Angle valve
 - Gate valves
 - Diaphragm valves
- Rotary valves
 - Butterfly valves
 - Ball valves
 - Plug valves





1-1-1. GLOBE VALVES- SINGLE SEAT

- The most famous control valve in industry.
- Tight shut off capability, Leakage less than 0.05%
- Fast to open or close
- Difficult to manufacture in small sizes
- Quite heavy







1-1-2. GLOBE VALVES- DOUBLE SEAT

- Larger capacity
- Naturally balanced
- Lower leakage class





1-1-3. GLOBE VALVES- 3 WAY

Mixing









1-1-4. GLOBE VALVES- NEEDLE VALVE

- Precise low flow control
- Pressure reducing







1-1-5. GLOBE VALVES- ANGLE VALVE

- Space limitation
- High pressure drop







1-2. GATE VALVES

- High flow capacity
- Higher leakage class
- ON/OFF applications
- Prone to erosion





1-3. DIAPHRAGM VALVES

- Very simple
- Often used for corrosive, slurry, and sanitary services







1-4. BUTTERFLY VALVES

- Highest capacity
- Low pressure drop
- Lower leakage class
- Under pressure rating # 300







1-5. BALL VALVES

- Quick, tight shutoff, high capacity, and require only a 1/4 turn to operate
- almost ¹/₂ price of globe valves

Normally used for on-off service (like emergency shutdown application).







1-5-1. BALL VALVES

- Full bore
- Reduced bore
- V-notch



全径流道形式 缩径流道形式 Full-bore Channel Type Reduced-bore Channel Type







1-5-2. BALL VALVES

Top entry

Top entry valves allow access from the top without removing the valve from the pipeline.

Side entry

For maintenance or replacement, it may be necessary to remove the valve from the pipeline.

The ball and internal components of side entry ball valves enter from the side of the valve body.







1-6. PLUG VALVES

- Similar to a ball valve except that a cylinder is used instead of a sphere
- More expensive but more rugged than a ball valve
- Require more torque to turn but still easy to actuate







1-7. CHECK VALVES

- Check valves are generally installed in pipelines to prevent backflow.
- A check valve is basically a one-way valve, in which the flow can run freely one way, but if the flow turns, the valve will close to protect the piping, other valves, pumps etc.





SWING CHECK VALVE



LIFT /PISTON CHECK VALVE







1-8. PRESSURE SAFETY VALVES

 A Pressure Safety Valve (PSV) is a type of valve used to quickly release gasses from equipment in order to avoid over pressurization and potential process safety incidents.







2. CONTROL VALVE

- The most common final control element in the process control industries is the control valve. The control valve manipulates a flowing fluid, such as gas, steam, water, or chemical compounds, to compensate for the load disturbance and keep the regulated process variable as close as possible to the desired set point.
- Control loop







2-1. INDUSTRIAL CONTROL LOOP

 Most control loops in industry are related to pressure, temperature, level and flow quantities. Their control valves are PV, TV, LV and FV respectively.







2-1. CONTROL LOOP EXAMPLES







2-2. CONTROL VALVE TYPES

Globe valves

- Butterfly valves



Fast opening globe 50% 1998 globe

50%

100%

100%

0%







2-3. CONTROL VALVE GENERAL COMPONENTS

- Valve body
- Actuator
- Positioner







2-4. CONTROL VALVES COMPONENTS

- Body
- Bonnet
- Yoke
- Stem
- Plug
- Seat ring
- Cage
- Packing







2-5. CONTROL VALVE THERMODYNAMIC BEHAVIOR









2-6. CONTROL VALVES STANDARDS

Standard	Description
IEC 60534	Control Valves Standards
ISA S 75.01	Flow Equation for Sizing Control Valves
ISA S 75.02	Control Valves Capacity Test Procedure
IEC 60534-8	Industrial-Process Control Valves
EEMUA 140	Noise Procedure Specifications
API 598	Valve Inspections and Testing



3-CONTROL VALVE BEHAVIORS

- Linear
- Quick opening
- Equal percentage

Туре	Equation [†]
Linear	V = P
Quick Opening	$V = \frac{10.0P}{\sqrt{\left(1.0 + 9.9 \times 10^{-3} P^2\right)}}$
Equal Percentage	$V = \frac{0.01P^2}{\sqrt{2.0 - 1.0 \times 10^{-8} P^4}}$

Where:

t

- P = Valve opening as a percentage of maximum opening
- V = Flow coefficient as a percentage of flow coefficient at maximum opening







3-1. CONTROL VALVE BEHAVIOR (DETERMINANT COMPONENTS)

Plug

The contoured plug is profiled valve plug to give linear, equal percentage or quick opening characteristics.



Cage

The cage provides exceptional stability to the plug even at very high differential pressure which eliminates vibration that could otherwise damage or destroy the valve.



QUICK OPENING

W0958/IL

LINEAR

W0959/IL

EQUAL PERCENTAGE

W0957/IL

3-1. CONTROL VALVE BEHAVIOR (DETERMINANT COMPONENTS)

Cage (Continue)

Stem

MEHRAZ

Plug

Cage

80% open

3-2. TYPE OF CONTROL VALVE PLUGS

3-3. GLOBE VALVES-(BALANCED OR UNBALANCED)

3-4. LEAKAGE CLASS

Class	Maximum allowable leakage rate	Test pressure drop
I	(no specification given)	(no specification given)
II	0.5% of rated flow capacity, air or water	45-60 PSI or max. operating
III	0.1% of rated flow capacity, air or water	45-60 PSI or max. operating
IV	0.01% of rated flow capacity, air or water	45-60 PSI or max. operating
V	0.0005 ml/min water per inch orifice size per PSI	Max. operating
VI	Bubble test, air or nitrogen	50 PSI or max. operating

4. CONTROL VALVE PROBLEMS

Flashing

Cavitation

Noise

Distance through valve

4-1. FLASHING

- The liquid pressure drops below the vapor pressure and remains as vapor at downstream.
- Flashing will cause choke flow condition to occur.
- In addition the vapor bubbles can also cause mechanical damage to the valve and piping system.

4-2. CAVITATION

The second stage is the collapse or implosion of those cavities (beyond the vena contracta) back into an all liquid state. The energy released by cavitating liquids can, under certain circumstances, cause physical damage of valve or piping components

4-2-1. STAGED PRESSURE DROP

 Multi stage trims can help manage high pressure drops and avoid cavitation. The range includes various options offering up to 30 stages of pressure drop.

4-3. CHOKED FLOW

 Choked flow is the point at which decreasing downstream pressure will not increase the flow through a valve. This typically happens in high differential applications in a high pressure control valve in gas back pressure or pressure reducing service.

$$\Delta P_{Choked} = F_L^2 (P_1 - F_F P_v)$$

$$F_F \simeq 0.96 - 0.28 (P_v/P_c)^{1/2}$$

- F_L: Pressure recovery factor
- F_F: Critical pressure ratio factor

4-4. NOISE

- High noise levels can cause pipe vibration and damage to downstream equipment
- The maximum noise level for each control valve shall be limited to 85 dBA for normal operation
- Noise above 110 dBA can destroy a valve very quickly

5. CONTROL VALVE SIZING

- Type of fluid
- Temperature of fluid
- Flow rate of fluid
- Viscosity of fluid
- Specific Gravity of fluid
- Inlet pressure (Upstream)
- Outlet pressure (Downstream) of fluid
- Delta P shutoff for actuator sizing
- Pipe size/Schedule
- Decide Flow Direction and characteristics
- Calculate Cv

5. CONTROL VALVE SIZING

5-1. CONTROL VALVE SIZING-(LIQUID SERVICES)

• CV is the number of US gallons per minute of water which pass through a given flow restriction with a pressure drop of 1 psi.

Measuring system	Flow equation	Unit (Flow)	Unit (Press.)	Unit (Density)	Relation with C _v
American	$Q = C_v \sqrt{\frac{\Delta P}{G_f}}$	gal/min	psi (lb/in²)	lb/ft³	1
Metric	$Q = K_v \sqrt{\frac{\Delta P}{G_f}}$	m³/h	bar	Kg/m³	$C_v = 1.156K_v$
SI	$Q = A_{\nu} \sqrt{\frac{\Delta P}{G_{f}}}$	m³/s	Pa	Kg/m³	$A_v = 2.4 \times 10^{-5} C_v$

5-2. CONTROL VALVE SIZING-(GAS SERVICES)

$$C_{v} = \frac{Q}{1360F_{P}P_{l}Y}\sqrt{\frac{G_{g}T_{l}Z}{x}}$$

$$Y = 1 - \frac{x}{3F_k x_T}; \ x = \frac{\Delta p}{P_l}; \ F_k = \frac{k}{1.4}$$

- k: Ratio of specific heats for gases
- F_k: Ratio of specific heats factor
- Y: Expansion factor for gases
- Z: Compressibility factor
- x_T: Critical pressure drop ratio factor

5-3. CONTROL VALVE SIZING

Table of ISA Formulas

		VALUE OF N1		
REMARKS	EQUATIONS	U.S.	SI	
LIQUID Turbulent and	$q_f = N_1 F_p C_v \sqrt{\frac{\Delta p}{G_f}}$	1.00	0.0865	
Non-Cavitating	$w_f = N_6 F_p C_v \sqrt{\Delta p \gamma}$	63.3	2.73	
	$q_{f} = N_{1}F_{Lp}C_{v}\sqrt{\frac{p_{1}.p_{vc}}{G_{f}}}$	1.00	0.0865	
54	$w_{f} = N_{6}F_{Lp}C_{v}\sqrt{\frac{p_{1}-p_{vc}}{G_{f}}}$	63.3	2.73	
Choked	$p_{vc} = F_F p_v$ $F_F = 0.96 - 0.28 \sqrt{\frac{p_v}{p_c}}$			
	$F_{LP} \approx \left[\frac{1}{F_{L^*}} + \frac{K_i}{N_2} \left(c_d \right)^* \right]^{-1/2}$	890	0.00214	
	K _i = (See Piping Geometry Factor)			
	$q_f = N_{10} \frac{\Delta p}{\mu} \left(F_s F_p C_v \right)^{3/2}$	52	173	
Laminar	$\mathbf{F}_{s} = \left(\frac{\mathbf{F}_{p}\mathbf{F}_{d}^{*}}{\mathbf{F}_{LP}}\right)^{1/3} \left[\frac{(\mathbf{F}_{LP}\mathbf{C}_{v})^{t}}{\mathbf{N}_{2}\mathbf{D}^{*}} + 1\right]^{1/6}$	890	0.00214	
Transitional	$q_f = N_1 F_R F_P C_v \sqrt{\frac{\Delta p}{G_f}}$	1.00	0.0865	

Table of ISA Formulas (continued)

REMARKS	EQUATIONS	VALUE OF N U.S. SI				
Gas or Vapor - (All Equations: $x \in F_k x_T$)						
	$w_g = N_6 F_p C_v Y \sqrt{x p_1 \gamma_1}$	63.3	2.73			
	$q_g = N_7 F_p C_v p_1 Y \sqrt{\frac{x}{G_g T_1 Z}}$	1360	4.17			
Variations for Selected units.	$w_g = N_8 F_p C_v p_1 Y \sqrt{\frac{xM}{T_1 Z}}$	19.3	0.948			
	$q_g = N_9 F_p C_v p_1 Y \sqrt{\frac{x}{MT_1 Z}}$	7320	22.4			
Expansion factor lower limit = 0.667	$Y = 1 - \frac{x}{3F_k xT}$					
Sp. ht. ratio factor	$F_{k} = k/1.40$	-				
Mfr's. Factors	$x_{T} = \frac{C_{1}^{z}}{1600} = 0.84C_{f}^{z}$					
\mathbf{x}_{T} with reducers	$x_{TP} = \frac{x_T}{F_p^*} \left[\frac{x_T K_i}{N_5} \left(C_d \right)^* + 1 \right]$ K _i = (See Piping Geometry Factor)	1 1000	0.0024			
<u></u>						
Steam (Dry and Saturated)						
For x < x _{Tp}	$w = NF_p C_{vP1} \left(3 - \frac{x}{x_{TP}}\right) \left(\sqrt{1 + \frac{x}{x_{TP}}}\right)$	x) 1.0	0.152			
For $x \ge xTp$ (Choked Flow)	$w = NF_p C_v p_1 \sqrt{x_{TP}}$	2.0	0.304			

¹U.S. units are: pounds per hour, gallons per minute, pounds per square inch absolute, pounds per cubic foot, °R, and inches.

SI units are: kilograms per hour, cubic meters per hour, kPa, kilograms per cubic meter, *K, and millimeters.

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5-3. CONTROL VALVE SIZING

Table of ISA Formulas (continued)

REMARKS	EQUATIONS	EQUATIONS			
Piping Geometry Fac For F _{LP} see "Liquid Choked Flow"	890 0.00214				
Sum of velocity head coefficients	$\sum \mathbf{K} = \mathbf{K}_1 + \mathbf{K}_2 + \mathbf{K}_{B1} - \mathbf{K}_{B2}$				
Bernoulli coefficient	$K_{B1} = K_{B2} = 1 \cdot \left(\frac{d}{D}\right)^*$				
Resistance coefficient for abrupt transitions	$K_1 = 0.5 \left[1 - \left(\frac{d}{D} \right)^2 \right]^2$				
Inlet fitting co- efficient for F _{LP} and ^x TP-	$K_{2} = 1.0 \left[1 \cdot \left(\frac{d}{D}\right)^{*} \right]^{*}$ $K_{i} = K_{1} + K_{B1}$				
Line Velocity	Feet/Second Meters/Second		Range (Ft/Sec.)		
Liquid	$U = \frac{q}{2.45D^2} \qquad U = 354 \frac{q}{D^2}$	}	5-10 Norm. 40-50 Max.		
Gas	$U = \frac{qT}{695pD^2} \qquad U = 1.24 \frac{qT}{pD^2}$	}	250-400		
Vapor	$U = \frac{W}{19.6\gamma D^2} \qquad U = 354 \frac{W}{\gamma D^2}$]	70 Wet		
Steam	$U = \frac{23w}{pD^2} \qquad U = 685 \frac{W}{pD^2}$]	300 superneated		
Acoustic Velocity (M	ach 1.0)				
Gas	$U_a = 223 \sqrt{\frac{kT}{M}} \qquad U_a = 91 \sqrt{\frac{kT}{M}}$	}	< 0.3 Mach		
Air	$U_a = 49 \sqrt{T}$ $U_a = 20 \sqrt{T}$	J			
Steam, Superheated	$U_a = 60 \sqrt{T}$ $U_a = 24.5 \sqrt{T}$	}	<0.15 Mach		
Steam, Dry Saturated	$U_a = 1650$ $U_a = 500$]	<0.10 Mach		
Vapor	$U_a = 68.1 \sqrt{kpv}$ $U_a = 1038 \sqrt{kpv}$]			

5-3. CONTROL VALVE SIZING

Nomenclature of ISA Formulas

a	Area of orifice or valve opening, in. ²
с	Coefficient of discharge, dimensionless. Includes effect of jet contraction and Reynolds number, mach number (gas at high velocities), turbulence.
Cd	Relative capacity (at rated C_v) $C_d = N_3 C_v / d^2$.
cp	Specific heat at constant pressure.
c _v	Specific heat at constant volume.
C _v	Valve coefficient, 38 a \overline{K}/F_{L} .
d	Valve inlet diameter, inches of mm.
D	Pipe diameter, inches or mm.
F	Velocity of approach factor = $\frac{1}{\sqrt{1-m^2}}$.
Fd	Experimentally determined factor relating valve $C_{\mathbf{v}}$ to an equivalent diameter for Reynolds number. (See Table IV)
f	Weight fraction
FF	Liquid critical pressure ratio factor, $F_F = p_{vc}/p_v$
Fk	Ratio of specific heats factor.
FL	Pressure recovery factor. When the valve is not choked:
	$F_{L} = \sqrt{(p_1 - p_2) / (p_1 - p_{vc})}$
FLP	Combined pressure loss and piping geometry factors for valve/fitting assembly.
FP	Correction factor for piping around valve (e.g. reducers) $F_P C_{\bf v}$ = effective $C_{\bf v}$ for valve/fitting assembly.
FR	Correction factor for Reynolds number, where F_RC_v = effective C_v .
Fs	Laminar, or streamline, flow factor.
g	Acceleration due to gravity.
Gf	Specific gravity of liquids at flowing temperature relative to water at 60°F or 15°C.
Gg	Specific gravity of gas relative to air with both at standard temperature and pressure.
h	Effective differential head, height of fluid.
ĸ	Flow coefficient=CF, dimensionless.
ΣК	Sum total of effective velocity head coefficients where $K(U^2/2g) = h$.
Kp	Bernoulli coefficient = $1-(d/D)^4$.

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Nomenclature of ISA Formulas (continued)

κ _c	Cavitation index. Actually the ratio $\Delta p/(p_1,p_v)$ at which cavitation measurably affects the value of $C_v.$
к _i	Inlet velocity head coefficient, $K_1 + K_{B1}$
K1	Resistance coefficient for inlet fitting.
к 2	Resistance coefficient for outlet fitting.
k	Ratio of specific heats of a gas = c_p/c_v , dimensionless.
М	Molecular weight.
m	Ratio of areas.
N	Numerical constant (See Table I)
р	Absolute static pressure.
Pc	Thermodynamic critical pressure
pr	Reduced pressure, p/pc
Pv	Vapor pressure of liquid at inlet
q	Volume rate of flow.
Rev	Reynolds number for a valve.
Т	Absolute temperature.
Tc	Thermodynamic critical temperature
Tr	Reduced temperature, T/Tc
U	Average velocity.
v	Specific volume (1/ γ).
w	Weight rate of flow.
x	Ratio of differential pressure to absolute inlet static pressure, x = (p_1 - p_2) / p_1
×T	Terminal or ultimate value of x, used to establish expansion factor, Y.
×TP	Value of x _T for valve/fitting assembly.
Y	Expansion factor. Ratio of flow coefficient for a gas to that for a liquid at the same Reynolds number (includes radial as well as longitudinal expansion effects).

5-4. CONTROL VALVE SIZING

Chocked Condition In gases:

$$x_T = \frac{1}{F_k} \left[\frac{dP_{ch}}{P_{in}} \right], F_k = \frac{C_P}{C_V}$$

Chocked Condition In Liquids:

$$F_{L} = \sqrt{\frac{(P_{1} - P_{2})}{(P_{1} - P_{VC})}}$$

*At approximately 70% of valve travel. Maximum valve capacity may be estimated using the values given in this figure in conjunction with Fig. 4-29. For a more detailed analysis of capacity capabilities of a given valve at other percentages of travel, consult the valve manufacturer's data.

6-ACTUATORS

- Actuator type
 - Manual
 - Pneumatic
 - Diaphragm
 - Piston
 - Single or double acting
 - Hydraulic
 - Electrical
- Fail conditions

6-1. ACTUATORS-MANUAL

FOR SLIDING-STEM VALVES

W8176-1

FOR ROTARY-SHAFT VALVES

6-2. ACTUATORS-PNEUMATIC DIAPHRAGM

- Direct action: Valve opens when driving power has failed.
- Reverse action: Valve closes when driving power has failed

6-3-1. ACTUATORS-PNEUMATIC PISTON

 A single-acting pneumatic actuator uses air to open the valve and a mechanical spring to close the valve.

Single Acting Cylinder

Push Type

6-3-2. ACTUATORS-PNEUMATIC PISTON

Double-acting actuators use air pressure to both open and close the valve.

6-3-3. HEIGHT COMPARISON (BETWEEN DIAPHRAGM AND PISTON ACTUATORS)

6-4. RACK AND PINION ACTUATORS

- Rack and pinion actuators are mechanical devices used to automatically open and close valves or dampers.
- "Rack and pinion" is a generic term for a pair of gears which convert linear motion into rotational motion.

6-5. ELECTRO HYDRAULIC ACTUATORS

 devices that operate a value through pressurized hydraulic fluid with the electrical source of energy.

6-6. ACTUATOR TYPES COMPARISON

	Pneumatic type	Hydraulic type	Motorized type
Response time	Dead time is rather long. Action speed is fast.	Dead time is short. Action speed is fast	No dead time. Action speed is slow
Maintaining safety position at supply fail time	Possible by using integrated spring or connecting volume tank easily and certainly.	Difficult to maintain	Can stop and maintain only the position at an emergency time.
Output power	Middle for spring diaphragm type. Big for piston cylinder type.	Small for oil integrated type. Big for oil separated installation type	Bigger than pneumatic type and oil pressure type
Structure	tructure Simple		Complicated
Weather proof and Exprosion proof	Not necessary	Should be considered	Should be considered
Air piping or electric wiring Simple		Simple for oil integrated type. Complicated for oil separated installation	Simple
Maintenance work	Easy	Complicated	Complicated
Cost	Reasonable	Expensive	Expensive

6-7. CTUATORS- FAIL CONDITIONS

- ATO Air To Open
- ATC Air To Close
- FLP Fail Last Position

Two port valves				
Actuator action Direct		Reverse	Reverse	Direct
Valve action	Valve action Direct		Direct	Reverse
On air failure	Valve opens		Valve	closes

6-7. ACTUATORS- FAIL CONDITIONS

7. POSITIONERS

- A positioner for a control valve receive signal from controller and converts the signal to the appropriate opening or closing setting of the valve based on a desired set point for a process variable, whether it be pressure, temperature, or flow. It provides the accurate control of the valve.
- A positioner ensures that there is a linear relationship between the signal input from the control system and the position of the control valve.
- This means that for a given input signal, the valve will always attempt to maintain the same position regardless of changes in valve differential pressure, stem friction, diaphragm hysteresis and so on.
- A positioner may be used as a signal amplifier or booster. It accepts a low pressure air control signal from controller and, by using its own higher pressure input, multiplies this to provide a higher pressure output air signal to the actuator diaphragm, if required, to ensure that the valve reaches the desired position.

7. POSITIONERS

PNEUMATIC

ANALOG (ELECTRO-PNEUMATIC / EP)

DIGITAL

7-1. POSITIONERS (A PNEUMATIC VALVE POSITIONER)

 A Pneumatic Valve Positioner receives a pneumatic signal from a controller. Accurate valve stem or shaft position proportional to the pneumatic input signal.

7-1. POSITIONERS (A PNEUMATIC VALVE POSITIONER)

7-2. POSITIONERS (ANALOG I/P POSITIONER)

 An Electro-Pneumatic or I/P (I-to-P) Positioner use a mix of both electricity signal and air pressure. It receives an electric signal from a controller, Convert the electronic current signal (4-20 mA DC signal) into a pneumatic pressure signal and send a corresponding pneumatic signal 3-15 psi or 0.2-1.0 bar to a pneumatic valve actuator.

7-3. POSITIONERS (DIGITAL VALVE POSITIONER)

 A digital valve positioner also receives an electric signal from a controller. But it is digital as opposed to analog. It then sends a corresponding pneumatic signal to a pneumatic valve actuator.

7-3. POSITIONERS (DIGITAL VALVE POSITIONER)

 It also differs from an EP because it uses a microprocessor to convert the control signal and perform the position control rather than a mechanical beam cam and flapper assembly found in an EP. This electrical input allows more advance capabilities for the users.

7-3. **POSITIONERS** (DIGITAL VALVE POSITIONER)

 These digital smart positioners also collect data to automatically alert users about valve performance, diagnostics and maintenance.

Microprocessor

Mechanical beam, cam and flapper assembly

8. VALVE ACCESSORY

- It A device that is mounted on the actuator to complement the actuator's function and make it a complete operating unit.
- Examples include:
- Positioners
- Supply pressure regulators
- Solenoids & Solenoid Valve Manifold
- Limit Switches
- Supply Pressure Regulator
- Pneumatic Lock-Up Systems
- Electro-Pneumatic Transducers

9. VALVE MATERIALS

- Valve body material selection is usually based on the Pressure, Temperature, Corrosive properties and Erosive Properties of the flow media.
- Cast Iron (ASTM A126) is used for steam. Water. Gas and non corrosive fluids and is inexpensive.
- Cast Bronze (ASTM B61& ASTM B62) is used for steam, Air, Water, Oil and non corrosive fluids.
- Cast carbon steel (ASTM A216-Grade WCB) is the most popular steel for valve bodies in moderate service such as Air, superheat or saturated steam, non corrosive fluids.
- Cast Chrome-Moly Steel (ASTM A217-Grade WCB-C9) has addition of chromium/Molybdenum that provide corrosion resistance and also is suitable for temperature up to 1050 Deg.F.
- Cast type 304 SST (ASTM A351-Grade CF8) is for oxidizing and very corrosive fluids.
- Cast type 316 SST (ASTM A351-Grade CF8M) is same as 304 SST but since it has addition of Molybdenum then better resistance to corrosion.

10. CONTROL VALVE SELECTION

- Select Valve type
- Select Higher Cv from available
- Select Valve size, trim size for available range
- End Conn. type (Flanged or Screwed) and rating selection
- Leakage class selection
- Material Selection
- Actuator selection
- Packing and bonnet type selection
- Valve Action (F.C. or F.O)
- Instrument Air Supply Pressure
- Accessories /Positioners/Etc. selection

SAMPLE DATASHEET

	CONTROL VALVE DATA SHEET									
1		TAG NO			P&I) NO. :	0. :			
2		FLUID:			SER\	/ICE				
3		UNITS			MA	X. FLOV	V NORM.FLOW	MIN.FLO	N SHUT-OFF	
4		FLOW RATE		KG/HR						
5	Z	INLET PRESSURE		BARA						
6	Ĕ	OUTLET PRESSURE		BARA						
7	ND	INLET TEMPERATURE		°C						
8	8	DENSITY@(PT)/SPEC.GRAV.@a	atm,15 C/MW	KG/M3						
9	E	VISCOSITY/ SPEC HEATS RATIO	CP/CV	cP/						
10	RV	VAPOR PRESSURE PV		BARA						
11	SE	LIQ CRITICAL PRESS.		BARA						
12		COMPRESSIBILITY FACTOR Z								
13		CALCULATED CV								
14		REQUIRED CV								
15		MAX. ALLOWED NOISE		dBA						
16		PIPE LINE NO.			43		TYPE			
17	NE	PIPE LINE SIZE: IN/OUT			44		SIZE	EFF AREA		
18		SCHEDULE: IN/OUT			45		ON/ OFF	MODULATIO	DN	
19		PIPE LINE INSULATION			46		SPRING ACTION TO OPEN/CLOSE			
20		ТҮРЕ			47	~	MAX. ALLOWABLE PRESSURE			
21		SIZE ANSI CLASS			48	01	MIN. REQUIRED PRESSURE			
22		MAX PRESS. Bara MAX. TEMP. OC			49	2	AVAILABLE AIR SUPPLY PRESS barg			
23	z	BODY/BONNET MATL			50	AC.	MAX.	MIN.		
24	10	LINER MATERIAL / ID			51		BENCH SET RANGE bar g			
25	.iq	END CONNECTIONS	IN		52					
26	ō		OUT		53		HANDWHEEL TYPE	HANDWHEEL TYPE		
27	Ш	FLG. FACE FINISH			54		AIR FAILURE VALVE	SET	AT	
28	. N	END EXT/MATL.			55		INPUT SIGNAL			
29	SEF	FLOW DIRECTION			56		ТҮРЕ			
30		TYPE OF BONNET			57	S	ON INCR SIGNAL O	UTPUT INCR/	DEACR	
31			DA GUILLO TU		58	<u> </u>	GAUGES		BY-PASS	
32		PACKING MATERIAL		ν <u>Ε</u>	59		CAM CHARACTERIS	SIC		
33		TIGHT SHUT-OFF REQUIRED (Y	es/noj :	3.L.:	60	10		DATI	NC	
34					61	SW			NG	
35			RATED TRAV	EL	62		ACTUATION POINT			
20		CHARACTERISTIC			60	ET	SUP / SET PRESSUR		UNINECTION SIZE:	
37	Σ	BALANCED/UNBALANCED			64	~ 07	FILTER	GAU	GE	
38	TRI	SELECTED Cv: FL: XR:			65	E.	HYDRO PRESSURE			
39		TRIM MATERIAL			66	TES	ANSI / FCI LEAKAGI	E CLASS		
40		SEAT MATERIAL			67					
41		CAGE/GUIDE MATERIAL			68	2	MANUFACTURER			
42		STEM MATERIAL			69	SC	MODEL NO.			
NOT	EC.	1					1			

NOTES:

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